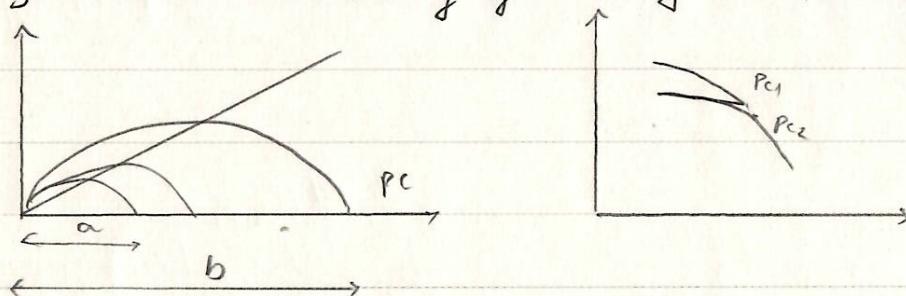


- In Modified Cam clay model, when the soil moves from overconsolidated state to the yield surface, soil obeys elastic stress-strain relationship. However as shown in experimental tests, plastic strain can be observed. Thus, there is a need to modify this model.

- The important feature to capture is that: plastic strain occurs all the time & as soil's OC state is far away from NCL, E^p is small compared with E^e and when soil's state is near NCL, E^p is larger in %.

- Hashiguchi proposed a subloading surface in which E^p can be determined by the ratio of the size between subloading yield surface & Yield surface^(a)



However, in real soil behavior (4) can be seen which ≠ preconsolidation pressure: $P_{c1} \neq P_{c2}$

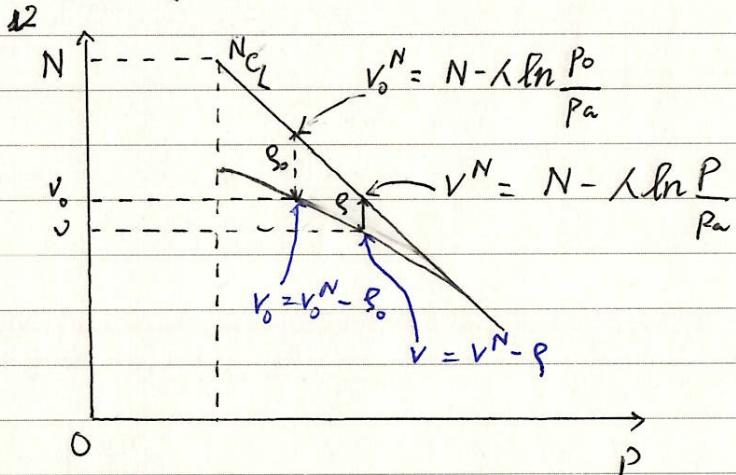
- Kikumoto $\frac{1}{2}$ proposed the state parameter.

$$\varphi = -\varphi_{\text{current}} + e_{\text{NCL at same } p}$$

- f is always = 0
- $\dot{\epsilon}^P$ always $\neq 0$
- Unloading \rightarrow elastic behavior only
- Reloading: $\dot{\epsilon}^P \neq 0$

Subloading Modified Cam Clay model ②

ρ small: $\dot{\epsilon}^P > \dot{\epsilon}^e$
 large: $\dot{\epsilon}^e > \dot{\epsilon}^P$



$$V_0 = V_0^N - \beta_0 = N - \lambda \ln \frac{P_0}{P_a} - \beta_0$$

$$V = V^N - \beta = N - \lambda \ln \frac{P}{P_a} - \beta$$

$$\Delta V = V - V_0 = -\lambda \ln \frac{P}{P_0} - (\beta - \beta_0)$$

$$\dot{\epsilon}_v = -\frac{\Delta V}{V_0} = \frac{\lambda}{V_0} \ln \frac{P}{P_0} + \frac{\beta - \beta_0}{V_0}$$

$$\dot{\epsilon}_v^e = \frac{K}{N_0} \ln \frac{P}{P_0}$$

$$\Rightarrow \dot{\epsilon}_v^P = \dot{\epsilon}_v - \dot{\epsilon}_v^e = \frac{\lambda - K}{V_0} \ln \frac{P}{P_0} + \frac{\beta - \beta_0}{V_0}$$

$$\Rightarrow f = \frac{\lambda - K}{V_0} \ln \frac{P}{P_0} + \frac{\beta - \beta_0}{V_0} - \dot{\epsilon}_v^P$$

Consistency Condition:

$$df = 0$$

$$\underbrace{\frac{\partial f}{\partial \sigma} d\sigma}_{\text{same as MCC}} + \underbrace{\frac{\partial f}{\partial \beta} d\beta}_{\substack{\frac{1}{V_0} \\ \text{Unknown}}} + \underbrace{\frac{\partial f}{\partial \dot{\epsilon}_v^P} d\dot{\epsilon}_v^P}_{\substack{-1 \\ \lambda \frac{\partial f}{\partial \sigma}}} = 0$$

Subloading Modified Cam Clay model

* The evolution law of state variable φ :

In constitutive model research, there are 2 main jobs:

- ① Find a reasonable variable
- ② Find its evolutional law

* Analysing process to find $d\varphi$.

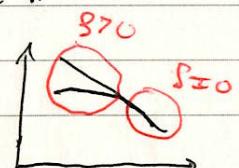
① When ε^P occurs, $\varphi \downarrow$

$$\Rightarrow d\varphi \sim - \|d\varepsilon^P\|$$

② If we directly use

$$d\varphi = - \|d\varepsilon^P\| \text{ then } \varphi \rightarrow < 0$$

\rightarrow not OK.



③ We use a modified version:

$$d\varphi = - \|d\varepsilon^P\| \varphi$$

. when $\varphi < 0$, very small $\Rightarrow d\varphi > 0$. Finally, $\varphi \rightarrow 0$

. when $\varphi > 0$, $\rightarrow d\varphi < 0$. Finally $\varphi \rightarrow 0$

④ To control the rate of convergence to 0, we use one more variable "a":

$$d\varphi = - a \|d\varepsilon^P\| \varphi$$

In practice, we use:

$$d\varphi = - a \|d\varepsilon^P\| \varphi \|g\|$$